# 1.5-GeV Proton FFAG as Injector to the BNL-AGS

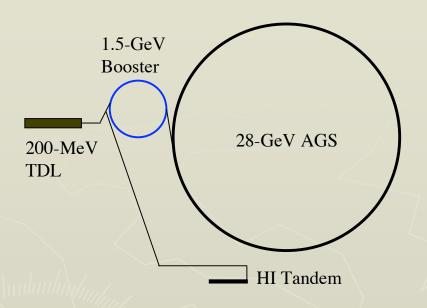
Alessandro G. Ruggiero
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N. Tsoupas, W. Zhang

**Brookhaven National Laboratory** 

FFAG 2004 Workshop, Vancouver, Canada. April 15-21 2004 Presentation to C-A Department, BNL. May 14, 2004 Invited Oral Contribution to EPAC 04. July 5-9, 2004

#### **Present BNL - AGS Facility**





#### **Performance**

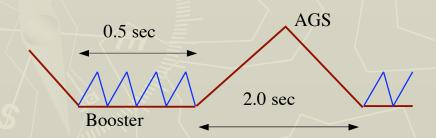
Rep. Rate 0.4 Hz

Top Energy 28 GeV

Intensity  $7 \times 10^{13} \text{ ppp}$ 

Ave. Power 125 kW

#### Typical AGS cycle for Protons



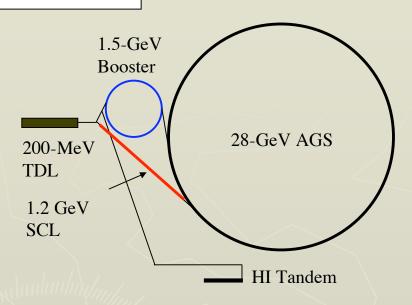
#### Typical DTL cycle for Protons



## **AGS Upgrade with 1.2-GeV SCL**



#### C-A/AP/151



#### **Performance**

Rep. Rate 2.5 Hz

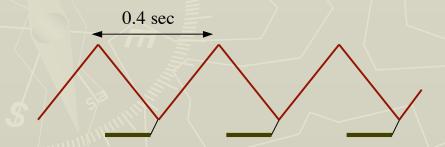
Top Energy 28 GeV

Intensity  $10 \times 10^{13} \text{ ppp}$ 

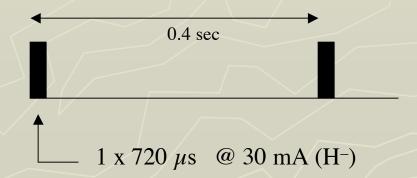
Ave. Power 1.0 MW

Only Protons, no HI

AGS Cycle with 1.2-GeV SCL



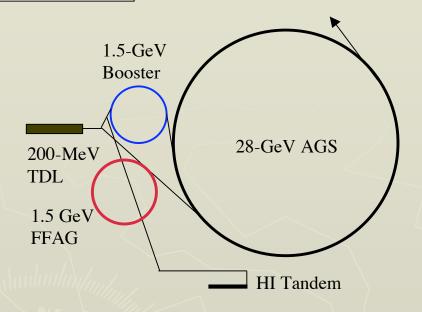
Typical DTL cycle for Protons



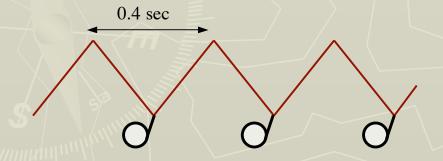
### **AGS Upgrade with 1.5-GeV FFAG**

F D F

#### C-A/AP/138



#### AGS Cycle with 1.5-GeV FFAG



#### **Performance**

Rep. Rate 2.5 Hz

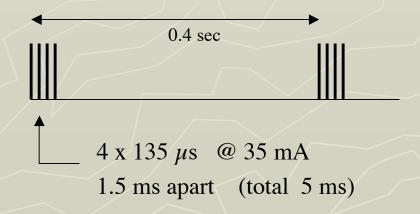
Top Energy 28 GeV

Intensity  $10 \times 10^{13} \text{ ppp}$ 

Ave. Power 1.0 MW

Protons, and HI

#### Typical DTL cycle for Protons



#### 1.5-GeV AGS FFAG



Table 1. Proton Beam Kinematic Parameters

	<u>Injection</u>	<u>Central</u>	Extract.
Kinetic Energy, MeV	200	786.722	1,500
β	0.5662	0.8391	0.9230
γ	1.213	1.838	2.599
Momentum, MeV/c	644.4	1,447	2,250
Magnetic Rigidity, kG-m	21.496	48.283	75.069
$\Delta p/p$	-0.5548	0.0	0.5548

Table 3. The AGS-FFAG Parameters for the Reference Trajectory

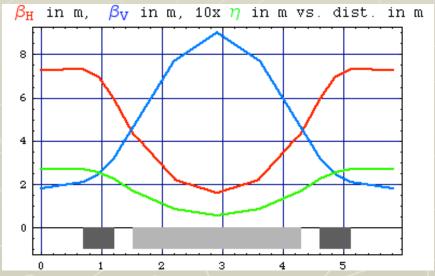
Circumference	244.439 m
Number of Periods	42
Period Length	5.81998 m
Short Drift, g	0.30 m
Long Drift, S	1.405954 m
Phase Advance / Period, H/V	97.7142° / 97.7142°
Betatron Tunes, H/V	11.40 / 11.40
Transition Energy, $\gamma_T$	39.7573 i



Table 2. Magnet Parameters

Magnet Type	F	D
Arc Length, m	0.509444	2.79514
Bending Field (B), kG	- 5.29169	4.51305
Gradient (G), kG/m	33.9174	-12.4036
Field Index, $n = G/Bh$	74.4451	-37.4293
Bend Radius ( $\rho = 1/h$ ), m	-10.2943	12.0705
Bending Angle, mrad	-49.4877	231.569
Sagitta, cm	0.355537	9.12532

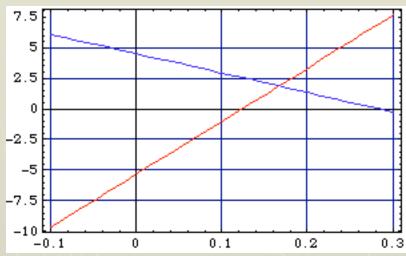
### Non-Scaling FDF Triplet



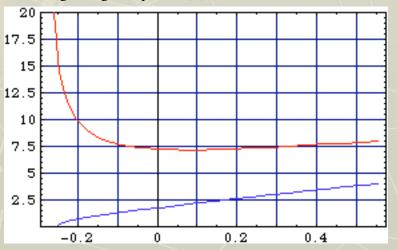
## Linear Field Profile (1 of 2)

F D F

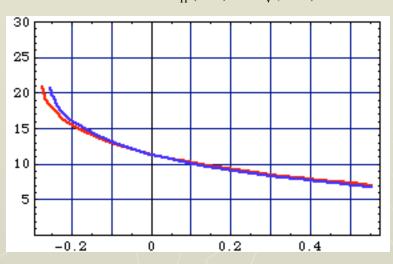
Field Profile (kG) vs. x (m) in F-Sector Magnet (Red) D-Sector Magnet (Blue)



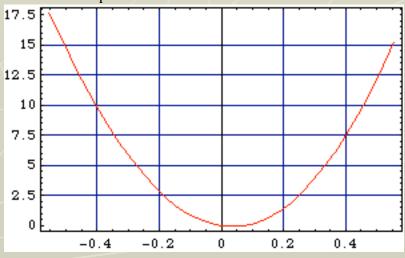
 $\beta_H$  (Red) and  $\beta_V$  (Blue) in m vs.  $\delta$  at the beginning of a period (S)



Tune variation vs.  $\delta = v_H (Red) = v_V (Blue)$ 



 $\Delta L$  in mm / period vs.  $\delta$ 



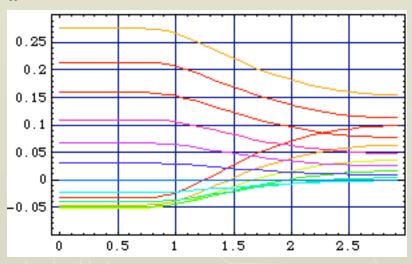
Friday, May 14, 2004

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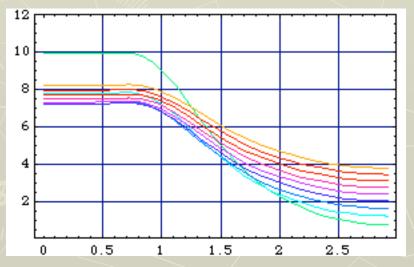
## Linear Field Profile (2 of 2)



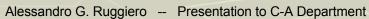
 $x_{co}$  (m) vs. period length (m) for  $\delta = -0.6$  to +0.6 in steps of 0.1



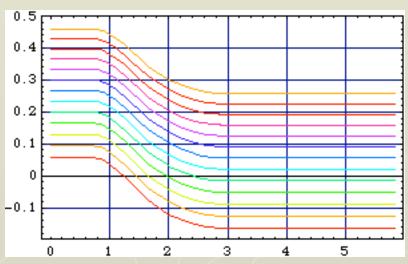
 $\beta_{\rm H}$  (m) vs. period length (m) for  $\delta = -0.6$  to +0.6 in steps of 0.1



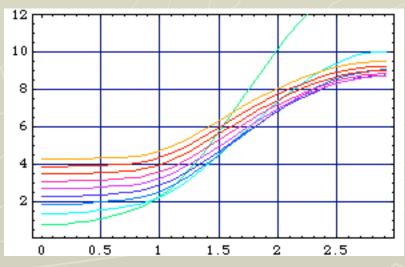
Friday, May 14, 2004



 $\eta$  (m) vs. period length (m) for  $\delta = -0.6$  to +0.6 in steps of 0.1

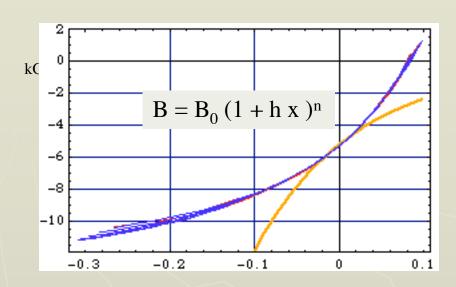


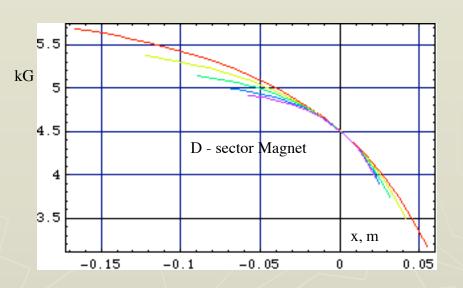
 $\beta_{\rm V}$  (m) vs. period length (m) for  $\delta = -0.6$  to +0.6 in steps of 0.1

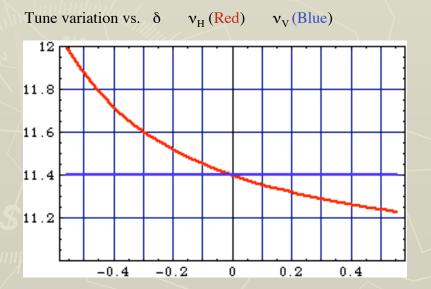


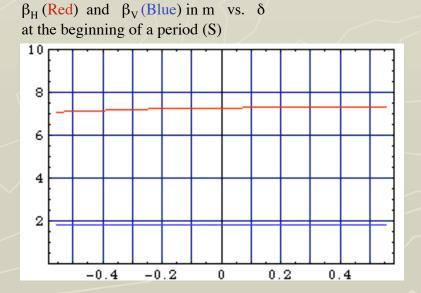
## Adjusted Field Profile (1 of 2)









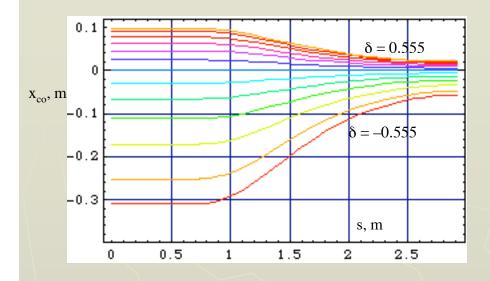


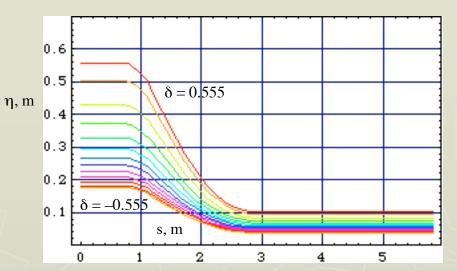
Friday, May 14, 2004

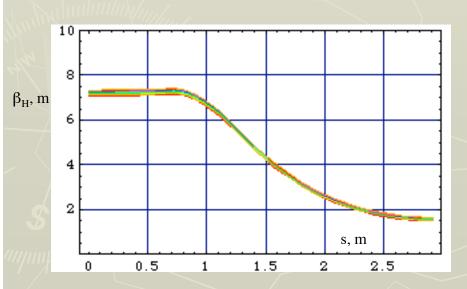
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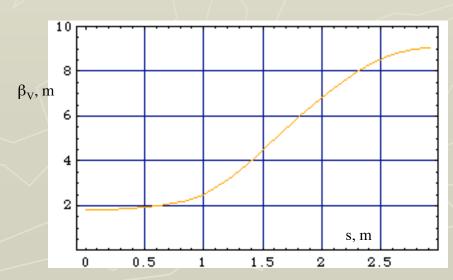












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#### Sandro's Recipe (1 of 3)

## F D F

#### C-A/AP/148

• Hamiltonian in Curvilinear Coordinate System (x, s, y)

$$H = -q A_s / c - (1 + h x) [p^2 - (p_x - q A_x / c)^2 - (p_y - q A_y / c)^2]^{1/2}$$

• (1) Expand square root

$$H = -q A_s / c - (1 + h x) p + (p_x - q A_x / c)^2 / 2 p + (p_v - q A_v / c)^2 / 2 p$$

- (2) <u>Drop higher order terms</u> like  $hx(p_x qA_x/c)^2$  and  $hx(p_y qA_y/c)^2$
- (3) Assume that the magnetic field is given solely by the longitudinal component  $A_s$  of the vector potential, whereas identically  $A_x = A_y = 0$

$$x'' = (q/pc) \partial A_s / \partial x + h$$
 <-- Curvature Function  $h = h(s)$   
 $y'' = (q/pc) \partial A_s / \partial y$ 

Magnetic Field Components

$$(1 + hx) B_y = \frac{\partial A_s}{\partial x} / \frac{\partial x}{\partial y}$$

$$(1 + hx) B_x = -\frac{\partial A_s}{\partial x} / \frac{\partial y}{\partial y}$$

### Sandro's Recipe (2 of 3)



• Equations of motion are now

$$x'' = (q / pc) B_y (1 + hx) + h$$
  
 $y'' = -(q / pc) B_x (1 + hx)$ 

• Quite generally  $B(z) = B_0 + G(z) z$ 

$$B = B_y + i B_x \qquad z = x + i y$$

$$B_x = \text{Imaginary } \{B(z)\}$$
 and  $B_y = \text{Real } \{B(z)\}$ 

• Motion on the y = 0 mid-plane

$$x'' = (q/pc)[B_0 + G(x)x](1 + hx) + h$$

• Lorenz Condition 
$$(q B_0 / p_0 c) = -h$$
 with  $p = p_0 (1 + \delta)$ 

## Sandro's Recipe (3 of 3)



- (4) Neglect the higher order term (q / pc) G h x<sup>2</sup>
- Introduce the *field index*  $n(x) = G(x) / h B_0$

$$x''$$
 +  $h^2 (1 + n) x / (1 + \delta)$  =  $h \delta / (1 + \delta)$   
 $y''$  -  $h^2 n y / (1 + \delta)$  = 0

• Consider the general case where the field index is a nonlinear function of both x and s, namely n = n(x, s). At any location s, for each momentum value  $\delta$  there is one unique solution  $x = x(\delta, s)$ , and by *inversion*  $\delta$  is a function of x and s, namely  $\delta = \delta(x, s)$ . We pose the following problem: Determine the field distribution, namely n = n(x, s), that compensates the momentum dependence of  $(1 + \delta)$  at the denominator:

$$n(x, s) = n_0 [1 + \delta(x, s)]$$
 -->  $G(x, s) = G_0 [1 + \delta(x, s)]$  <-- where  $n_0$  is related to the gradient  $G_0 = n_0$  h  $B_0$  on the reference trajectory.

• Then the equations of motion reduce to

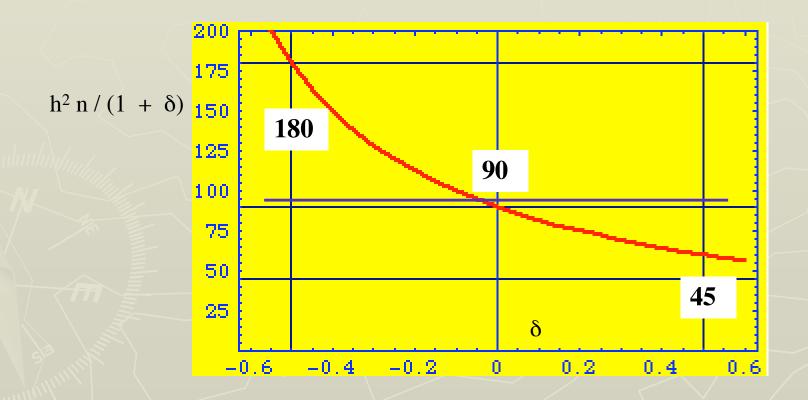
$$x'' + h^2 x / (1 + \delta) + h^2 n_0 x = h \delta / (1 + \delta)$$
 ->  $x = x(\delta, s)$  ->  $\delta = \delta(x, s)$   
 $y'' - h^2 n_0 y = 0$ 

• WARNING: (5) A variation with s of the guiding field introduce a *solenoid component* that must be evaluated and taken into account in the particle dynamics.

### **Chromaticity with Linear Gradient**



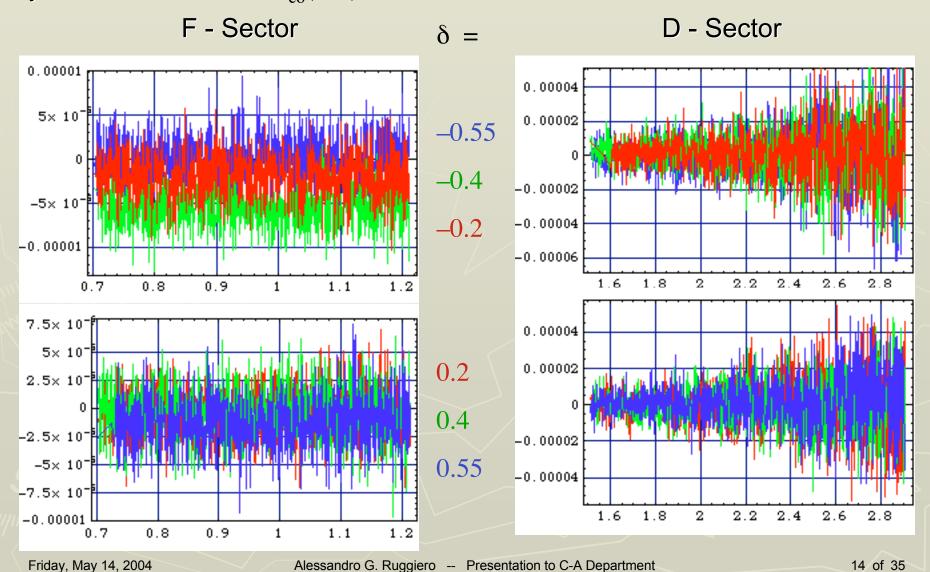
$$x''$$
 +  $h^2 (1 + n) x / (1 + \delta)$  =  $h \delta / (1 + \delta)$   
 $y''$  -  $h^2 n y / (1 + \delta)$  = 0



#### Proof of Sandro's Recipe (1 of 2)



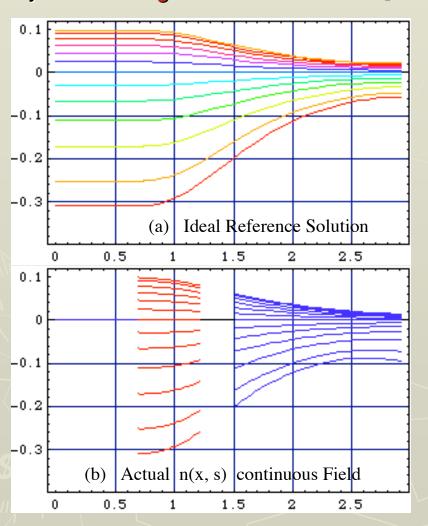
By Direct Substitution of  $x_{co}(\delta, s)$  in  $x'' + h^2 [1 + n(x, s)] x / (1 + \delta) = h \delta / (1 + \delta)$ 

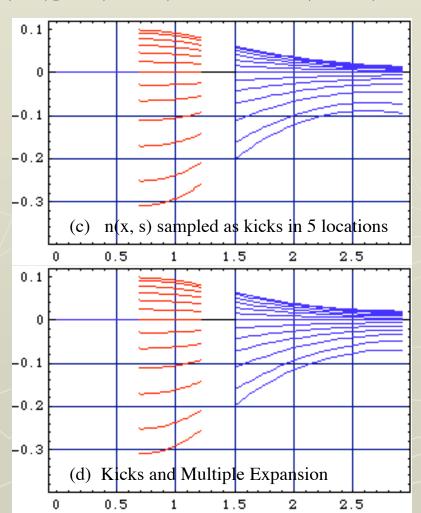


## Proof of Sandro's Recipe (2 of 2)



By Direct Integration of  $x'' + h^2 [1 + n(x, s)] x / (1 + \delta) = h \delta / (1 + \delta)$ 





#### **Alternative Solutions**



Other solutions are also possible. For instance, in order to flatten entirely the  $\delta$ -dependence of the horizontal betatron tune, one can set the field profile so that

1 + 
$$n(x, s) = (1 + n_0)[1 + \delta(x, s)]$$

leading to the equations of motion

$$x''$$
 +  $h^2 (1 + n_0) x$  =  $h \delta / (1 + \delta)$   
 $y''$  -  $h^2 [\delta / (1 + \delta) + n_0] y$  = 0

There is now a (reduced)  $\delta$ -dependence of the vertical betatron tune.

There is, of course, still dispersion on the horizontal plane.

The field profile on the y = 0 mid-plane associated to this solution is given by

$$B(x, s) = B_0 + G_0 [1 + \delta(x, s) (1 + 1/n_0)]$$

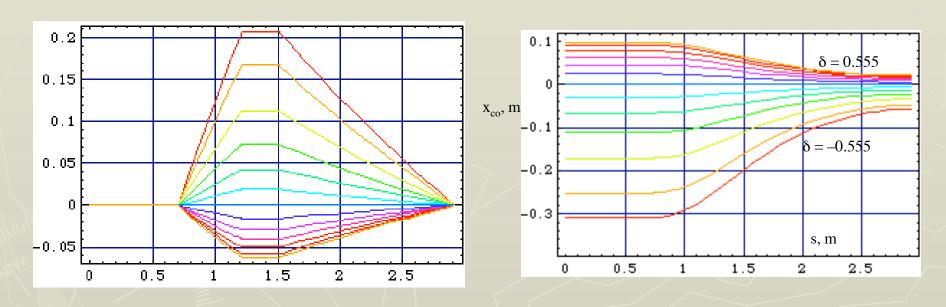
that, as long  $n_0 >> 1$ , is only slightly different from the previously derived field profile.

If desired, always in the search for an optimum cancellation of the chromatic and dispersive behavior, intermediate solutions can be found.

## Edge Effect (1 of 2)



 $x_{co}'$  in rad versus path length s in meter, for  $\delta = \pm 0.555$ 



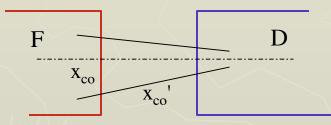
#### **MATHEMATICA**

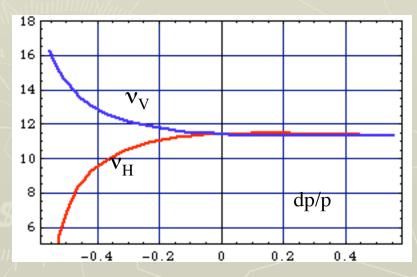
Presentation to C-A Department June 4, 2004

## Edge Effect (2 of 2)

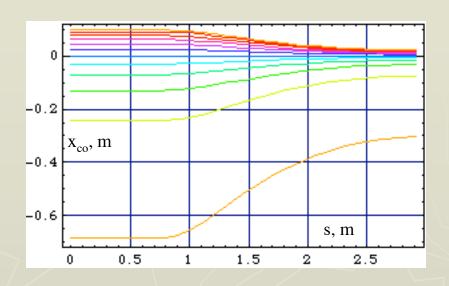
$$\Delta y' = - \frac{h_i B_i(x_{co})}{B_i (1 + \delta)} (\tan x_{co}') y$$

Vertical == Focusing
Horizontal == Defocusing





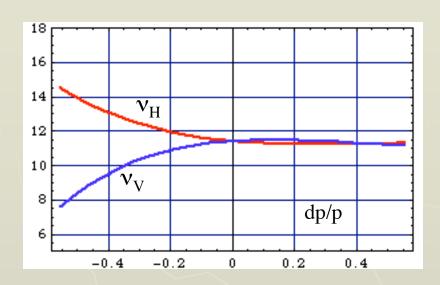


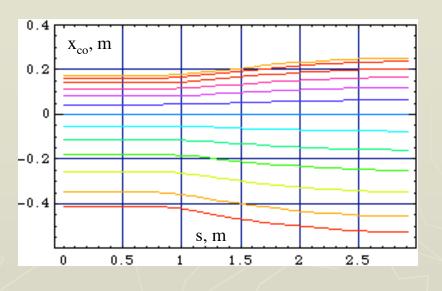


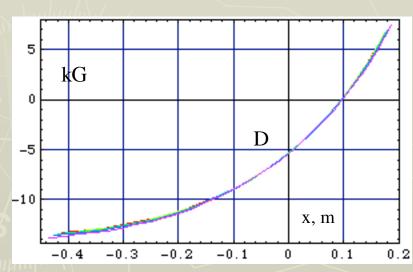
- Edge Effect is important and it cannot be neglected. In the case of the FDF-triplet arrangement there is a problem for large <u>negative</u> values of  $\delta$ .
- If we accept the *recipe* for the **Adjusted Field Profile**, we could also apply it to the DFD-triplet arrangement. Maybe in this case the problem will shift to large <u>positive</u> values of  $\delta$  (let us check!...)
- I am aware that the DFD-triplet is desirable for the accommodation of injection/extraction components and RF cavities, but it could make the central magnet wider.

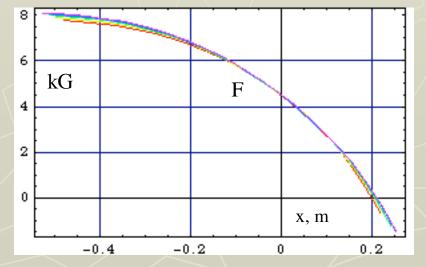
## **DFD** - Triplet





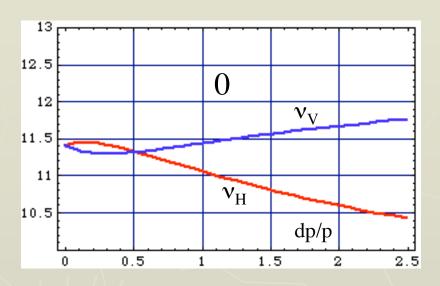


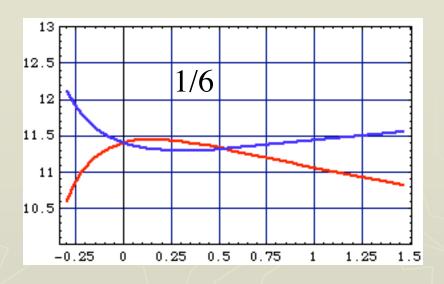


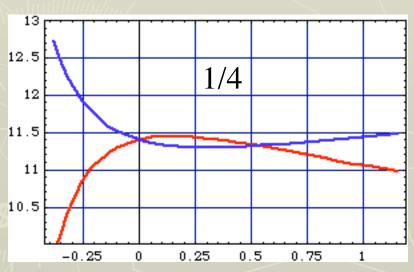


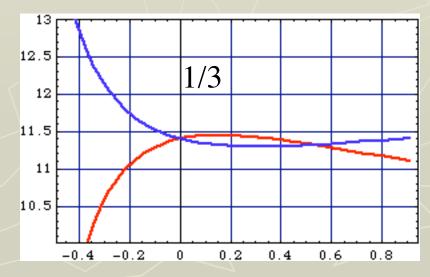
## Reference Trajectory (1 of 2)





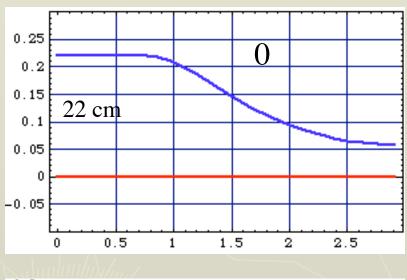


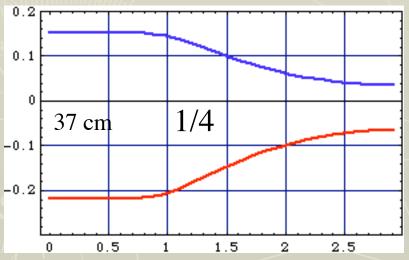


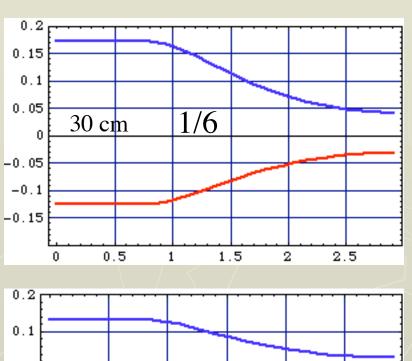


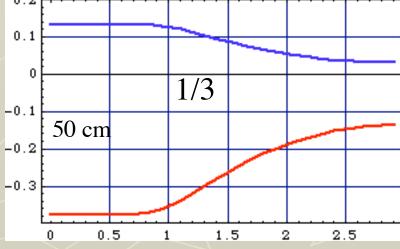
## Reference Trajectory (2 of 2)





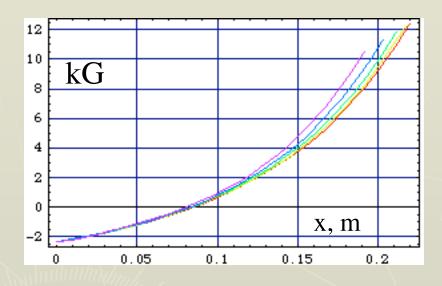






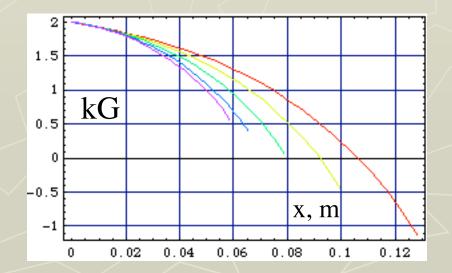
## Field Profile for ref traj at $\delta = 0$





<-- F - Magnet





#### Two instead of One



#### Single Ring:

200 MeV - 1,500 MeV

200 MeV - 1,200 MeV

200 MeV - 1,000 MeV

#### Δp/p

±0.555

±0.498

±0.449

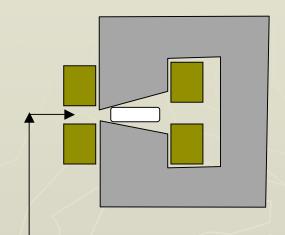
#### **Double Rings:**

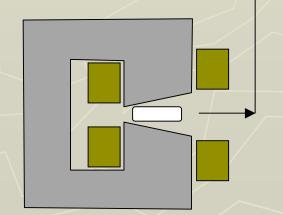
200 MeV - 600 MeV

600 MeV - 1,500 MeV

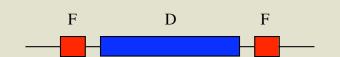
±0.308

±0.297



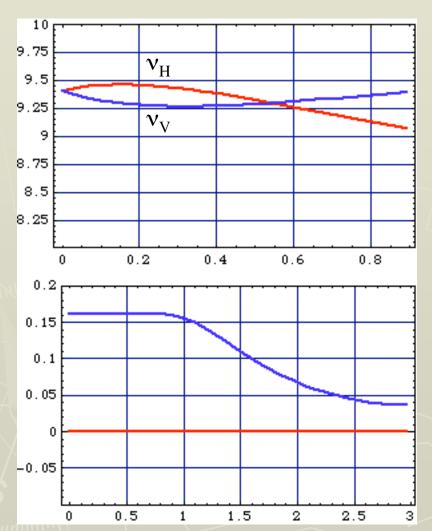


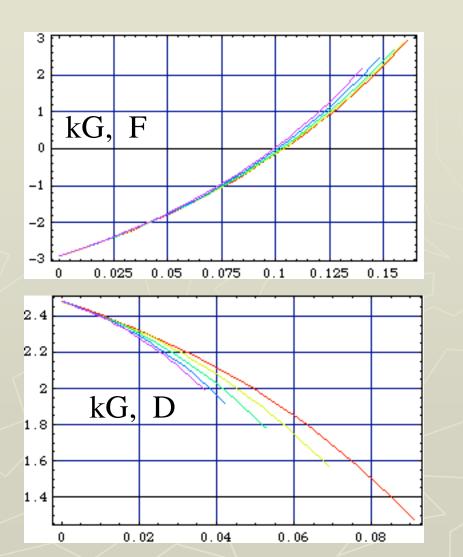
#### 1st FFAG 200 - 600 MeV





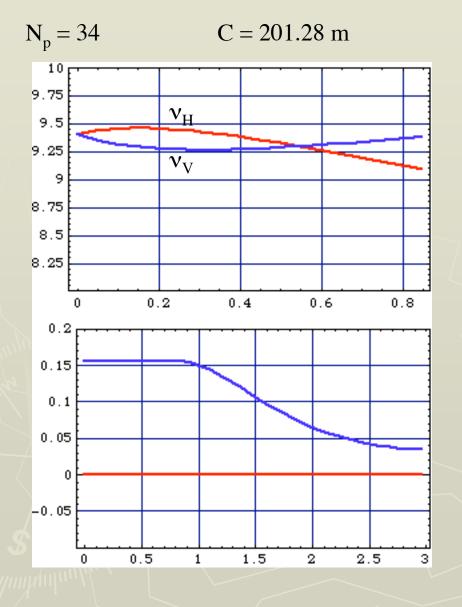
$$C = 195.36 \text{ m}$$

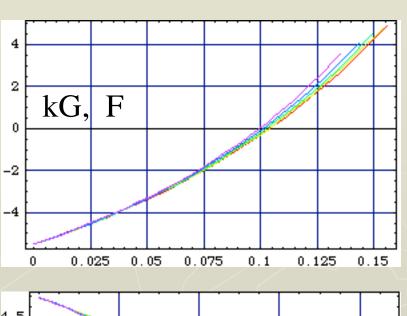


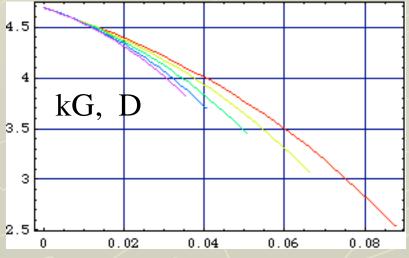


#### 2nd FFAG 600 - 1,500 MeV



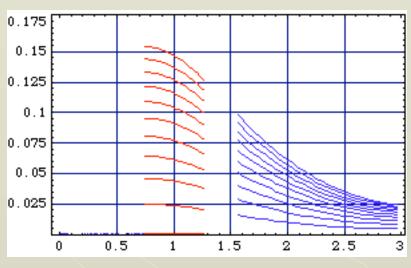


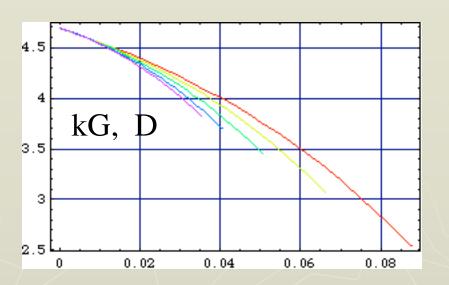


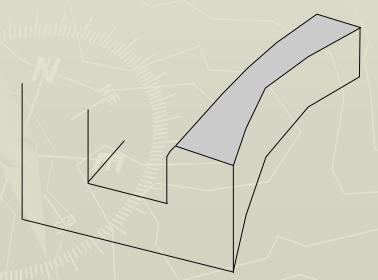


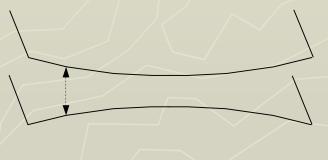






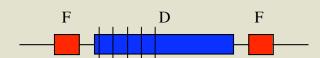






Minimum Gap 10 cm Maximum Width 15 cm

#### Multiple Expansion



```
tablen1 = Table[{x, ffB21[x]}, {x, tblsc2[0, 1], tblsc2[1, 1], 1/100}];
        f21 = FindFit[tablen1, B2 - G2 x + 50 (a12 x x /2! + a13 x x x /3! + a14 x x x x /4! + a15 x x x x x /5!) /L2, {a12, a13, a14, a15}, x]
        f1dB21[x_{1}] := B_{2} - G_{2}x + 50(a12xx/2! + a13xxx/3! + a14xxxx/4! + a15xxxxx/5!)/L_{2}/. f21;
        tablen2 = Table[{x, ffB22[x]}, {x, tblsc2[0, 2], tblsc2[1, 2], 1/100}];
        f22 = FindFit[tablen2, B<sub>2</sub> - G<sub>2</sub> x + 50 (a22 x x / 2! + a23 x x x / 3! + a24 x x x x / 4! + a25 x x x x x / 5!) / L<sub>2</sub>, {a22, a23, a24, a25}, x]
        fldB22[x_] := B2 - G2 x + 50 (a22 x x / 2! + a23 x x x / 3! + a24 x x x x / 4! + a25 x x x x x / 5!) / L2 /. f22;
        tablen3 = Table[{x, ffB23[x]}, {x, tblsc2[0, 3], tblsc2[1, 3], 1/100}];
        f23 = FindFit[tablen3, B<sub>2</sub> - G<sub>2</sub> x + 50 (a32 x x / 2! + a33 x x x / 3! + a34 x x x x / 4! + a35 x x x x x / 5!) / L<sub>2</sub>, {a32, a33, a34, a35}, x]
        f1dB23[x_{1}] := B_{2} - G_{2}x + 50(a32xx/2! + a33xxx/3! + a34xxxx/4! + a35xxxxx/5!)/L_{2}/. f23;
        tablen4 = Table[{x, ffB24[x]}, {x, tblsc2[0, 4], tblsc2[1, 4], 1/100}];
        f24 = FindFit[tablen4, B2 - G2 x + 50 (a42 x x /2! + a43 x x x /3! + a44 x x x x /4! + a45 x x x x x /5!) / L2, {a42, a43, a44, a45}, x]
        f1dB24[x_{]} := B_2 - G_2 x + 50 (a42 x x / 2! + a43 x x x / 3! + a44 x x x x / 4! + a45 x x x x x / 5!) / L_2 /. f24;
        tablen5 = Table[{x, ffB25[x]}, {x, tblsc2[0, 5], tblsc2[1, 5], 1/100}];
        f25 = FindFit[tablen5, B2 - G2 x + 50 (a52 x x /2! + a53 x x x /3! + a54 x x x x /4! + a55 x x x x x /5!) / L2, {a52, a53, a54, a55}, x]
        f1dB25[x_] := B_2 - G_2 x + 50 (a52 x x / 2! + a53 x x x / 3! + a54 x x x x / 4! + a55 x x x x x x / 5!) / L_2 /. f25;
        \{a12 \rightarrow -4, 232655311713346, a13 \rightarrow -89, 59973089484862, a14 \rightarrow -953, 1506613580015, a15 \rightarrow 6791, 009144574469\}
        \{a22 \rightarrow -5.685262451055018, a23 \rightarrow -175.6891898844062, a24 \rightarrow -1223.845907095543, a25 \rightarrow 40861.41277040269\}
        \{a32 \rightarrow -7, 621158731065018, a33 \rightarrow -333, 0805211091171, a34 \rightarrow -996, 6210049149577, a35 \rightarrow 269605, 4705855781\}
        \{a42 \rightarrow -9.956071799401875, a43 \rightarrow -494.4575260830500, a44 \rightarrow -16977.38138153995, a45 \rightarrow 2.750155386705654 \times 10^6\}
        \{a52 \rightarrow -11.74124249008848, a53 \rightarrow -654.2919120120293, a54 \rightarrow -22141.28562687770, a55 \rightarrow 4.591141269769532 \times 10^6\}
       bplt21 = Plot[{ffB21[x], fldB21[x]}, {x, tblsc2[0, 1], tblsc2[1, 1]},
               PlotStyle \rightarrow \{\{Hue[0.0], Thickness[0.007]\}, \{Hue[0.7], Thickness[0.007]\}\}, Frame \rightarrow True, Image True, 
        bplt22 = Plot[{ffB22[x], fldB22[x]}, {x, tblsc2[0, 2], tblsc2[1, 2]},
               PlotStyle \rightarrow {{Hue[0.0], Thickness[0.007]}, {Hue[0.7], Thickness[0.007]}}, Frame \rightarrow True, Imag.
       bplt23 = Plot[{ffB23[x], fldB23[x]}, {x, tblsc2[0, 3], tblsc2[1, 3]},
                PlotStyle \rightarrow {\{\text{Hue}[0.0], \text{Thickness}[0.007]\}, \{\text{Hue}[0.7], \text{Thickness}[0.007]\}\}, Frame \rightarrow True, Image
                                                                                                                                                                                                                                                                               kG, D
       bplt24 = Plot[{ffB24[x], fldB24[x]}, {x, tblsc2[0, 4], tblsc2[1, 4]},
               PlotStyle \rightarrow {{Hue[0,0], Thickness[0,007]}, {Hue[0,7], Thickness[0,007]}}, Frame \rightarrow True, Imag. 4
       bplt25 = Plot[{ffB25[x], fldB25[x]}, {x, tblsc2[0, 5], tblsc2[1, 5]},
               PlotStyle \rightarrow \{\{Hue[0.0], Thickness[0.007]\}, \{Hue[0.7], Thickness[0.007]\}\}, Frame \rightarrow True, Image (Proposition of the Control of
        Show[bplt21, bplt22, bplt23, bplt24, bplt25, Frame → True, ImageSize → 300, GridLines → Automat
                                                                                                                                                                                                                                                                  3
3.5
                                                                                                                                                                                                                                                                                                                                                                                                      x, m
                                                                                                                                                                                                                                                                                                             0.02
                                                                                                                                                                                                                                                                                                                                                    0.04
                                                                                                                                                                                                                                                                                                                                                                                            0.06
                                                                                                                                                                                                                                                                                                                                                                                                                                    0.08
                          0.02
                                               0.04
```

# Acceleration: Frequency Modulation



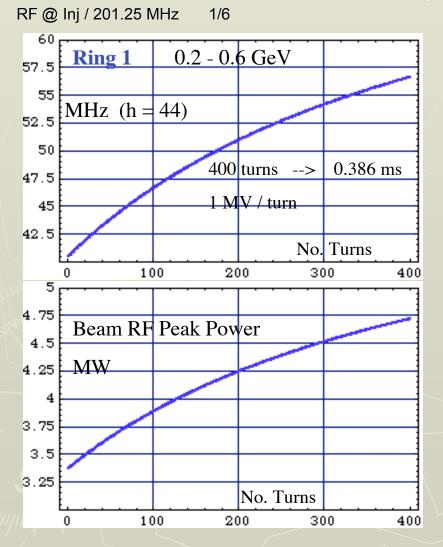
No. of Protons / pulse

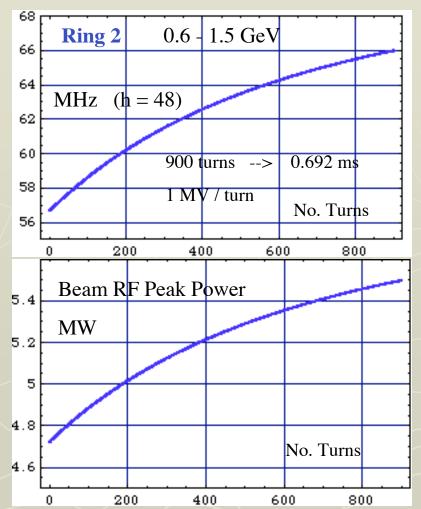
 $2.5 \times 10^{13}$ 

Single-Gap Cavity:

1.2 m long 50-100 kV

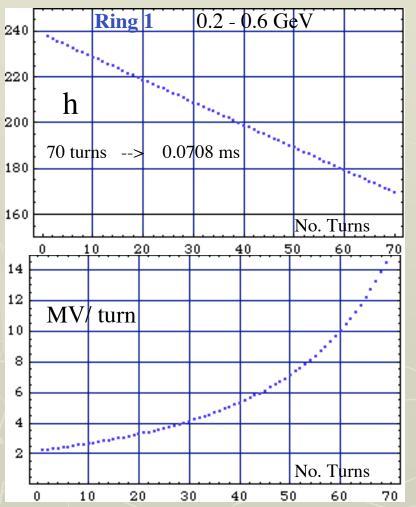
W: 20 cm H: 10 cm





# Acceleration: Voltage Modulation

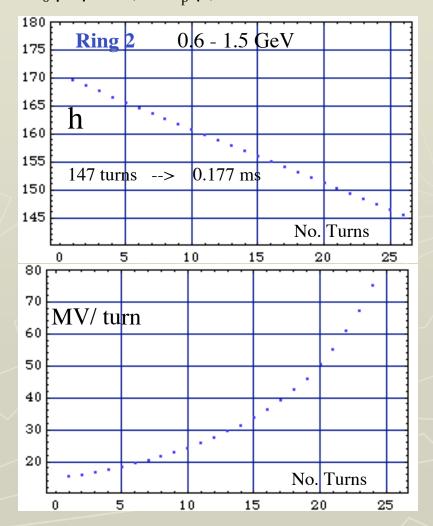
Constant RF 201.25 MHz



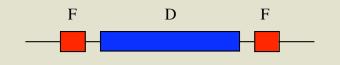


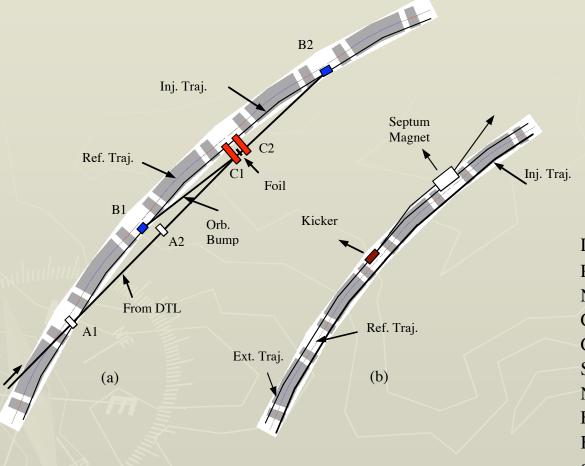
$$\Delta f / f = (1 / \gamma^2 - \alpha_p) \Delta p / p = -\Delta T / T = 1 / h$$

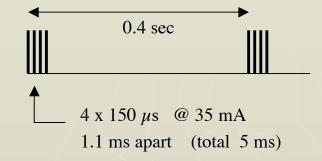
$$eV = E_0 \beta^2 \gamma^3 / h (1 - \alpha_p \gamma^2)$$



## Injection (H<sup>-</sup>) & Extraction







Linac Peak Current	35 mA
Rev. Period	$1.44~\mu \mathrm{s}$
No. Protons / pulse	$2.5 \times 10^{13}$
Chopping Ratio	80 %
Chopping Frequency	0.694 MHz
Single Pulse Duration	$144 \mu s$
No. inj. Turns / pulse	100
Emittance, rms norm.	$1 \pi$ mm mrad
Bunching Frequency	201.25 MHz
$\sigma_{\rm p}/p$	0.1 %

#### What to do Next....

F D F

Injector Requirements. Beam Pulse Formation.

Injector - FFAG Transport. Matching.

Multi-Turn Injection (H<sup>-</sup>, Charge Exchange).

Single-Turn Extraction. Transport and Matching to AGS.

RF Capture in the AGS.

Space-Charge Limitation at Injection.

Control of Beam Losses: Halo Formation, Activation....

Instabilities...

Interaction with Residual Vacuum Gas.

RF Acceleration: Frequency vs. Amplitude Modulation

#### **Beam Loading**

Two Rings versus One Ring.

Transfer between Rings. Matching.

Acceleration of Heavy Ions (!?)

Magnet Design and Manufacture.

Beam Control, Diagnostic, Steering,...

Tune Control. Resonance Crossing.

Beam Abort, Dump.

Computer Tracking. Analytical Work. MATHEMATICA

#### **Cost Estimate**

#### **Conclusions**

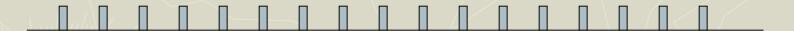


We have done a considerable amount of work.

We have launched new concepts and ideas.

We have made few inventions.

We need now to protect our Work....!



By extrapolation, it is also a continuous high power Proton Driver for a variety of applications:

Final Energy 1.5 GeV

Repetition Rate 670 Hz

Protons / Pulse 2.5 x 10<sup>13</sup>

Average Beam Power 4.0 MWatt

## **Acceleration of Heavy Ions**



#### **Protons**

Kinetic Energy, MeV	200	600	1,500
β	0.56616	0.79244	0.92300
γ	1.21316	1.63948	2.59870
p, MeV/c	644.44	1,218.98	2,250.51
Bρ, kG-m	<b>21.496</b>	<u>40.661</u>	·-···► <b>75.069</b> -

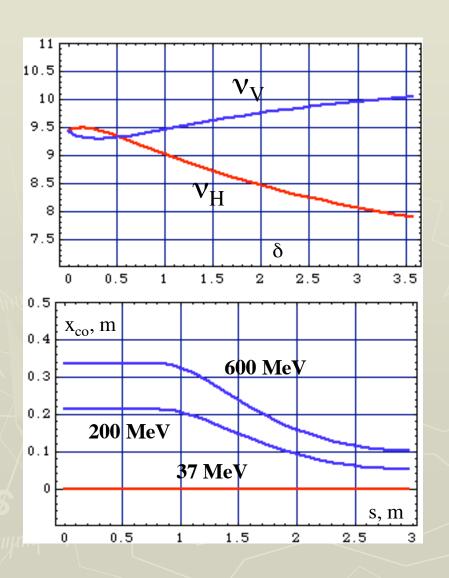
#### Gold lons (Au)

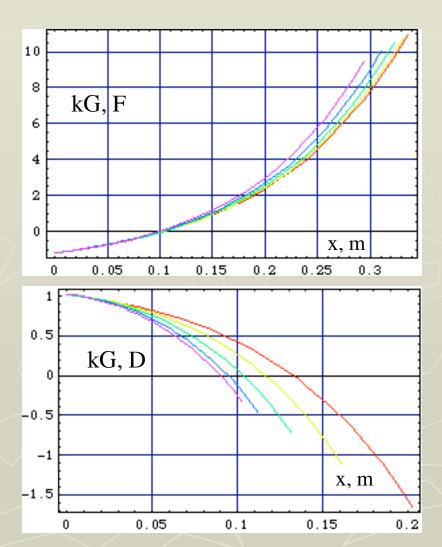
i \ \		
1.066	22	350
0.04781	0.21360	0.68682
1.00114	1.02362	1.37583
44.57	203.62	879.99
8.875	40.55	<u>175.23</u>
	0.04781 1.00114 44.57	0.04781       0.21360         1.00114       1.02362         44.57       203.62

A = 197 Z = 79 Q = +33

## Heavy Ions -- Ring 1







## Heavy Ions -- Ring 2



